- In the present invention, a compact burner
- 2 chamber employing a radiant burner assembly is
- 3 configured to distribute radiant energy along the
- 4 axial length of a tubular reaction chamber. In one
- 5 embodiment, the radiant burner assembly comprises a
- 6 woven metal fiber attached to a support structure that
- 7 permits the efflux of fuel and oxidant from the burner
- 8 core to the outer surface of the metal fiber. The
- 9 properties of the metal fiber stabilize the combustion
- 10 in a shallow zone proximal to the outer surface of the
- 11 metal fiber. The combustion reaction heats the metal
- 12 fiber to incandescence and provides a source of
- 13 radiant energy that is transferred to the reaction
- 14 chamber. In another embodiment, the radiant burner
- 15 assembly comprises a porous ceramic fiber burner that
- 16 accomplishes the same object by serving as a radiant
- 17 source of energy.
- The metal fiber of the burner typically
- 19 consists essentially of an alloy containing
- 20 principally iron, chromium, and aluminum and smaller
- 21 quantities of yttrium, silicon, and manganese having
- 22 extended life at operating temperatures up to 2000°F.

- In one embodiment, the tubular reaction
- 2 chamber has U-shape, and is sometimes referred to as a
- 3 hairpin tube, which is substantially filled with
- 4 catalyst, the tube extending into and out of the
- 5 combustion chamber for gaseous flow through. The
- 6 radiant burner axis is preferably vertically disposed
- 7 within the combustion chamber and oriented parallel to
- 8 the axis or axes of the U-tube reaction chamber. The
- 9 active radiant surface of the cylindrical radiant
- 10 burner assembly is defined by a geometric arc that
- 11 bisects the cylindrical assembly so as to maximize the
- 12 flux of radiant energy that is directed to the surface
- 13 of the U-tube reaction chamber. In this embodiment,
- 14 the center to center spacing between the radiant
- 15 burner and the U-tube reaction chamber, and the
- 16 radiation angle of the radiant burner are
- 17 simultaneously controlled, or configured for high
- 18 efficiency of heat transfer.
- 19 In a third embodiment, the tubular reaction
- 20 chamber comprises a helical coil that is substantially
- 21 filled with catalyst and has inlet and outlet portions
- 22 that pass into and out of the combustion chamber. The
- 23 helical coil is wrapped to form turns at specific lead

- 1 angles, so that the coil free area is in the range of
- 2 50% to 75%, wherein the free area is defined by the
- 3 ratio of the free area between helical tube conduits
- 4 or turns and the cylindrical surface that bisects the
- 5 helical coil circle or cylinder. The radiant burner
- 6 axis is typically vertically disposed within the
- 7 combustion chamber and the cylindrical radiant burner
- 8 is located at the center of the helical coil. In this
- 9 embodiment, the active radiant surface of the
- 10 cylindrical radiant burner assembly is defined by a
- 11 360-degree arc.
- In each embodiment, the radiant burner is
- 13 operated at a combustion intensity and an excess air
- 14 ratio that is carefully controlled to limit the
- 15 radiant burner surface temperature to less than 2000°F,
- 16 and preferably in the range of 1500°F to 1900°F, in
- 17 order to provide extended life for the radiant burner.
- 18 In each embodiment, the catalyst particle
- 19 diameters and reactant mass velocities are carefully
- 20 controlled to simultaneously limit the reactor
- 21 pressure drop to less than 8 psi, and preferably in
- 22 the range of 2 psi to 4 psi in order to limit the